

A finite-volume solution to the geophysical electromagnetic forward problem using unstructured grids

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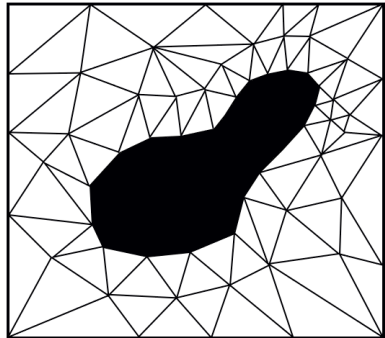
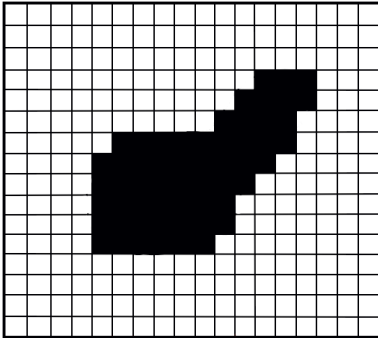
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- 1 Unstructured grids
- 2 A finite-volume discretization of Maxwell's equations
- 3 Example for magnetic dipole sources
- 4 Example for a long grounded wire source
- 5 Some accuracy studies
- 6 Conclusions

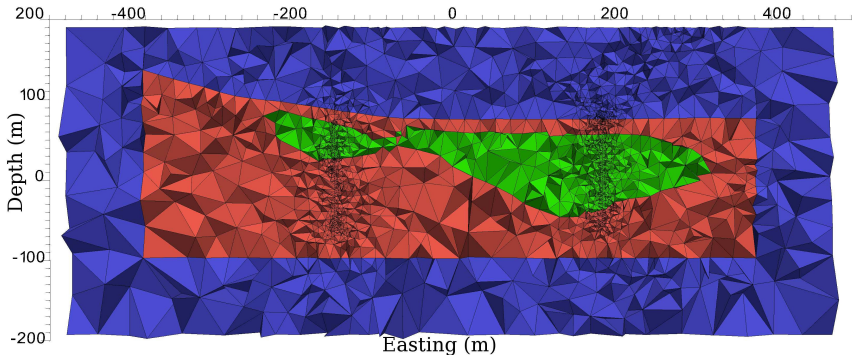
Unstructured grids

- Model irregular structures



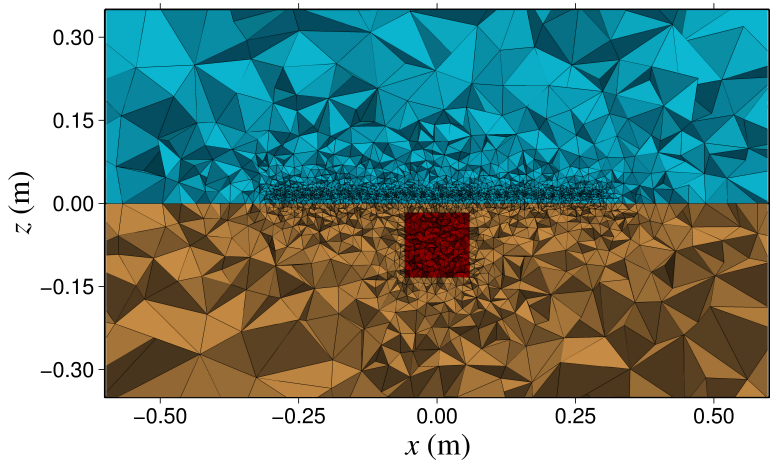
Unstructured grids

- Topographical features
- Geological interfaces



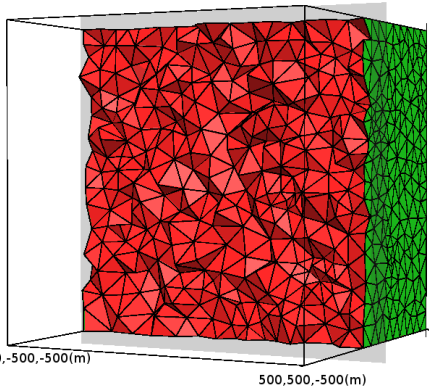
Unstructured grids

- Local refinement (at observation points, sources, interfaces)

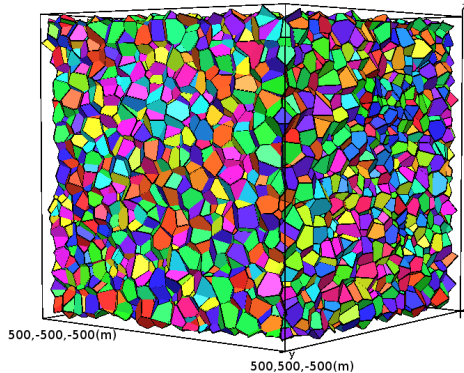


Dual tetrahedral-Voronoi grids

- Grid generator: TetGen (Si, 2004)



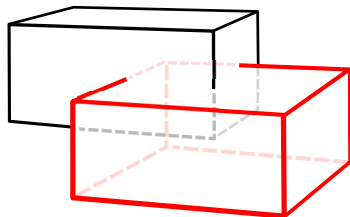
tetrahedral grid



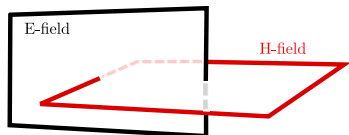
Voronoi grid

Staggered finite-volume schemes

- Magnetic field divergence free
- Easy for implementing boundary conditions
- Satisfies the continuity of tangential E
- Physically meaningful

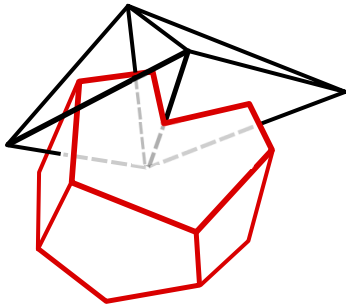


Rectilinear dual grid

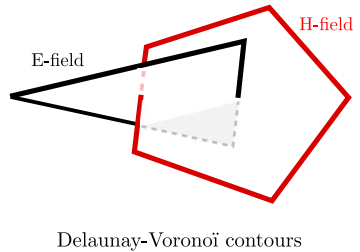


Rectilinear dual contours

Staggered finite-volume schemes



Dual tetrahedral-Voronoi grid



Delaunay-Voronoi contours

- **Maxwell's equations:**

$$\nabla \times \mathbf{E} = -i\omega\mu_0\mathbf{H} - i\omega\mu_0\mathbf{M}_p$$

$$\nabla \times \mathbf{H} = \sigma\mathbf{E} + \mathbf{J}_p$$

Helmholtz equation for electric field

$$\nabla \times \nabla \times \mathbf{E} + i\omega\mu_0\sigma\mathbf{E} = -i\omega\mu_0\mathbf{J}_p - i\omega\mu_0(\nabla \times \mathbf{M}_p)$$

- **Homogeneous Dirichlet boundary condition:**

$$\mathbf{E} = 0 \quad \text{at } \infty$$

or

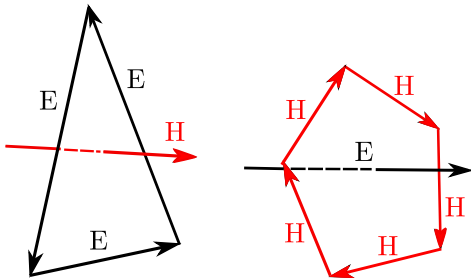
$$\mathbf{E} \cdot \boldsymbol{\tau} = 0 \quad \text{on } \Gamma$$

General features of the finite volume method

- Naturally supports unstructured grids
- Simple in idea
- Uses the integral form of equations
- Uses the average values of quantities

- Integral form of Maxwell's equations:

$$\oint_{\partial A^D} \mathbf{E} \cdot d\mathbf{l}^D = -i\mu_0\omega \iint_{A^D} \mathbf{H} \cdot d\mathbf{A}^D - i\mu_0\omega \iint_{A^D} \mathbf{M}_p \cdot d\mathbf{A}^D$$
$$\oint_{\partial A^V} \mathbf{H} \cdot d\mathbf{l}^V = \sigma \iint_{A^V} \mathbf{E} \cdot d\mathbf{A}^V + \iint_{A^V} \mathbf{J}_p \cdot d\mathbf{A}^V$$

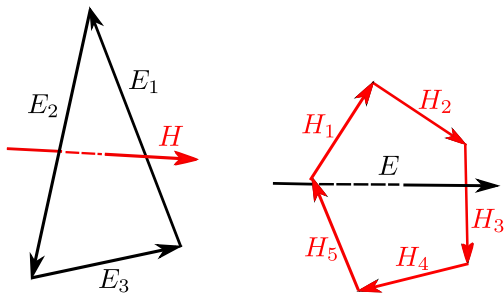


Finite-volume discretization

- Discretized form of Maxwell's equations:

$$\sum_{q=1}^{w_j^D} E_{i(j,q)} I_{i(j,q)}^D = -i\mu_0\omega H_j A_j^D - i\mu_0\omega M_{p_j} A_j^D$$

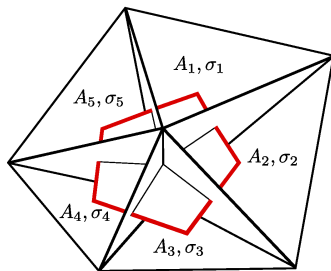
$$\sum_{k=1}^{w_i^V} H_{j(i,k)} I_{j(i,k)}^V = \sigma E_i A_i^V + J_{p_i} A_i^V.$$



Discretized Helmholtz equation

- Discretized form of Helmholtz equation:

$$\sum_{k=1}^{w_i^V} \left(\left(\sum_{q=1}^{w_j^D} E_{i(j,q)} I_{i(j,q)}^D \right) \frac{I_{j(i,k)}^V}{A_{j(i,k)}^D} \right) + i\omega\mu_0\sigma E_i A_i^V$$
$$= -i\omega\mu_0 \sum_{k=1}^{w_i^V} M_{pj(i,k)} \frac{I_{j(i,k)}^V}{A_{j(i,k)}^D} - i\omega\mu_0 J_{p_i}$$



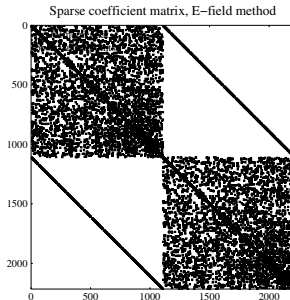
Finite-volume discretization

- Decompose E to real and imaginary parts:

$$E = E_{re} + iE_{im}$$

- Resulting block matrix equation:

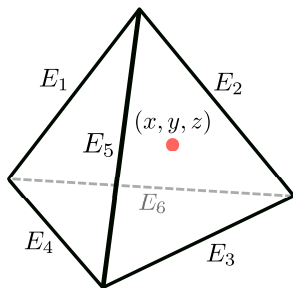
$$\begin{pmatrix} \mathbf{A} & -\mathbf{B} \\ \mathbf{B} & \mathbf{A} \end{pmatrix} \begin{pmatrix} \mathbf{E}_{re} \\ \mathbf{E}_{im} \end{pmatrix} = \begin{pmatrix} \mathbf{S}_{im} \\ \mathbf{S}_{re} \end{pmatrix},$$



Finite-volume discretization

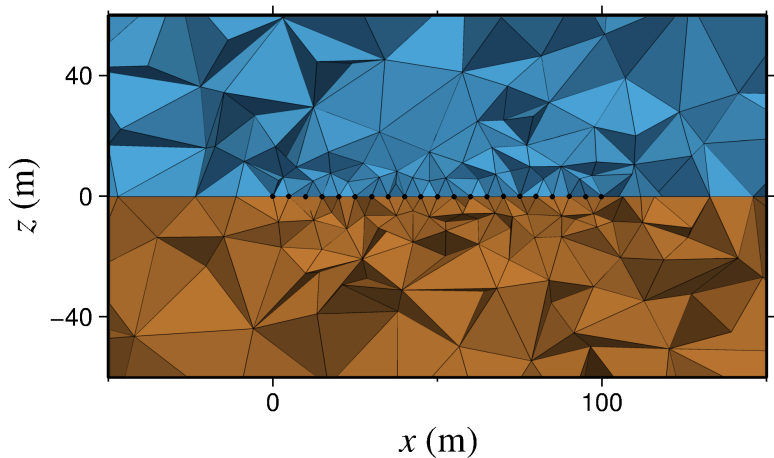
- Sparse direct solver: MUMPS (Amestoy et. al, 2006)
- Interpolation inside tetrahedra: vector basis functions

$$\mathbf{E}(x, y, z) = \sum_{i=1}^6 \mathbf{N}_i(x, y, z) E_i,$$



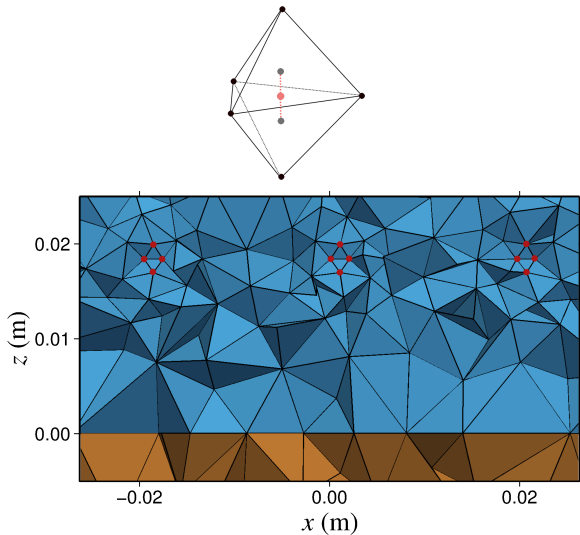
Inclusion of EM sources

- Grounded wire:



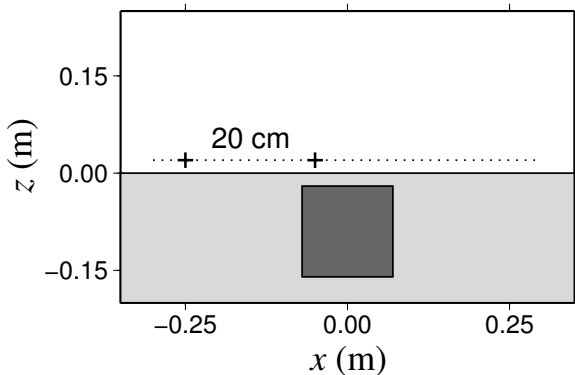
Inclusion of EM sources

- Point vertical magnetic dipole:



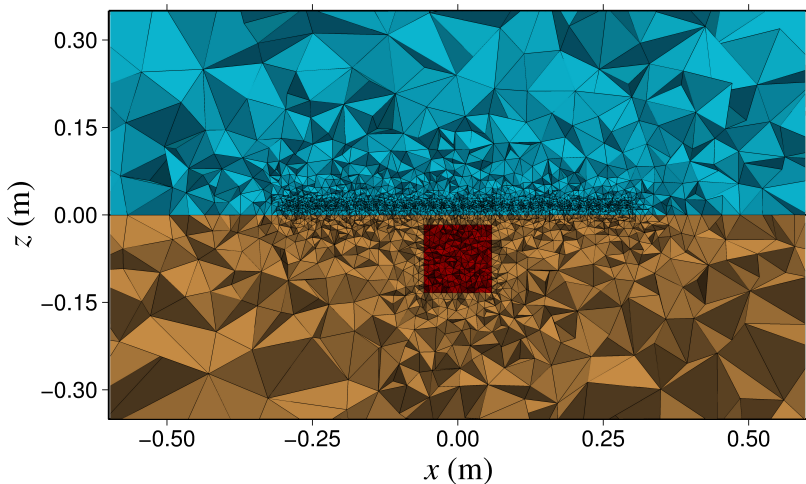
Example 1: magnetic dipole transmitter-receiver pairs

- Graphite cube in brine (physical scale modelling measurements)
- Transmitter-receiver pairs along the x axis at $z = 2 \text{ cm}$
- Dimensions of the cubic graphite: $14 \times 14 \times 14 \text{ cm}$
- $\sigma_{brine} = 7.3 \text{ S/m}$; $\sigma_{prism} = 63,000 \text{ S/m}$
- Frequencies: 1, 10, 100, 200, 400 kHz



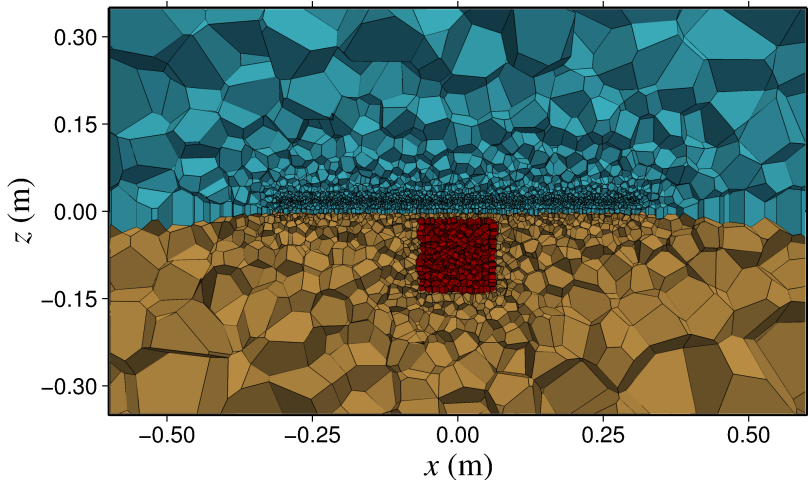
Example 1: magnetic dipole transmitter-receiver pairs

- Grid refined at the sources, observation points and the prism



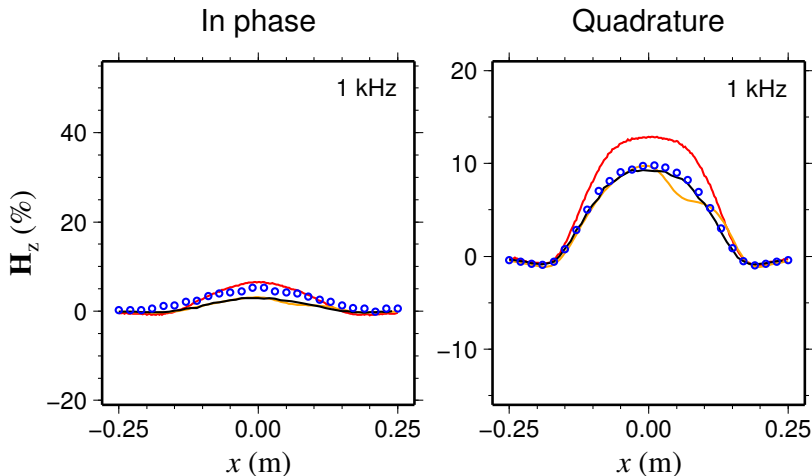
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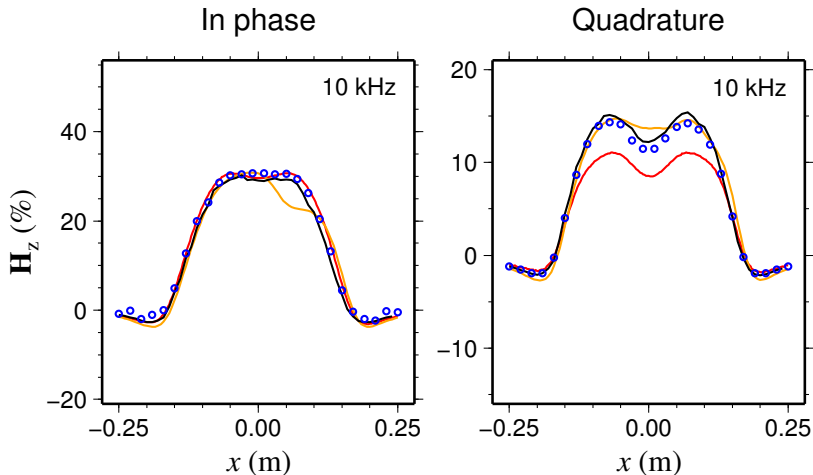
Example 1: magnetic dipole transmitter-receiver pairs

- Scattered H-field: (total–free-space)/free-space
- FV (circles) vs PSM (red), IE (orange), and FE (black)



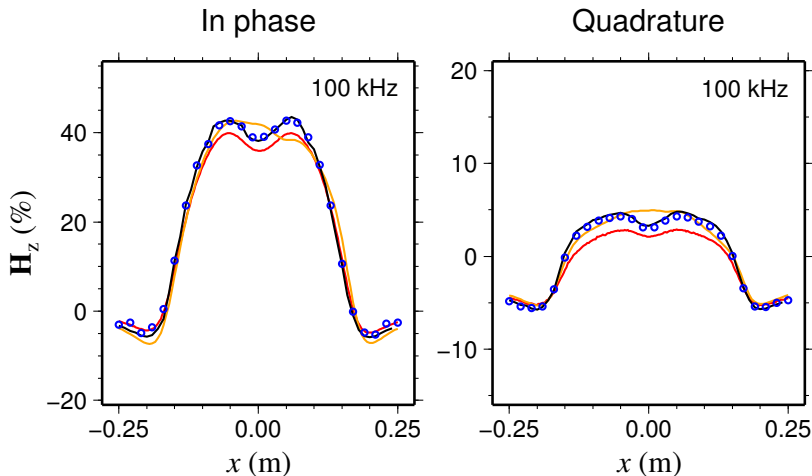
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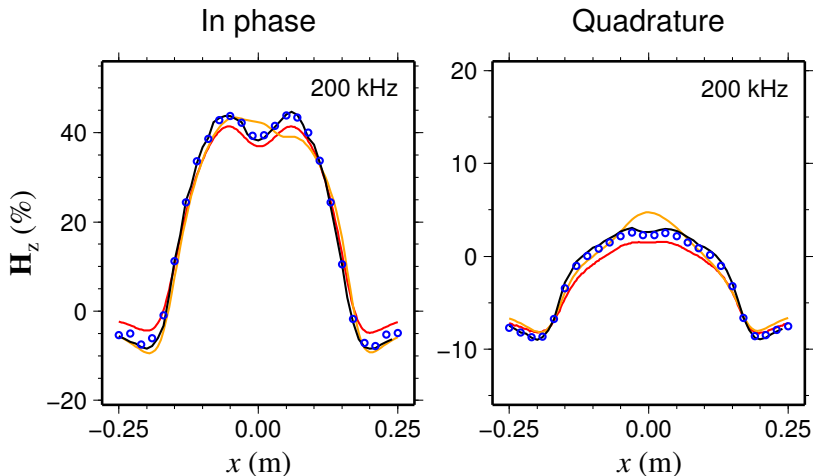
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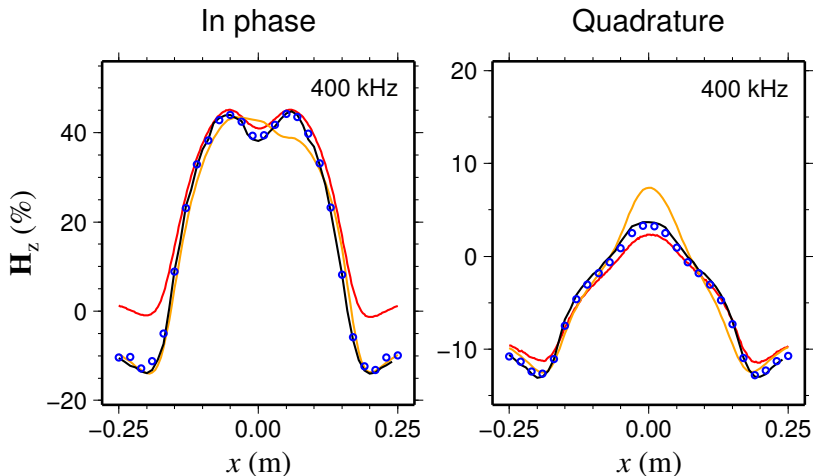
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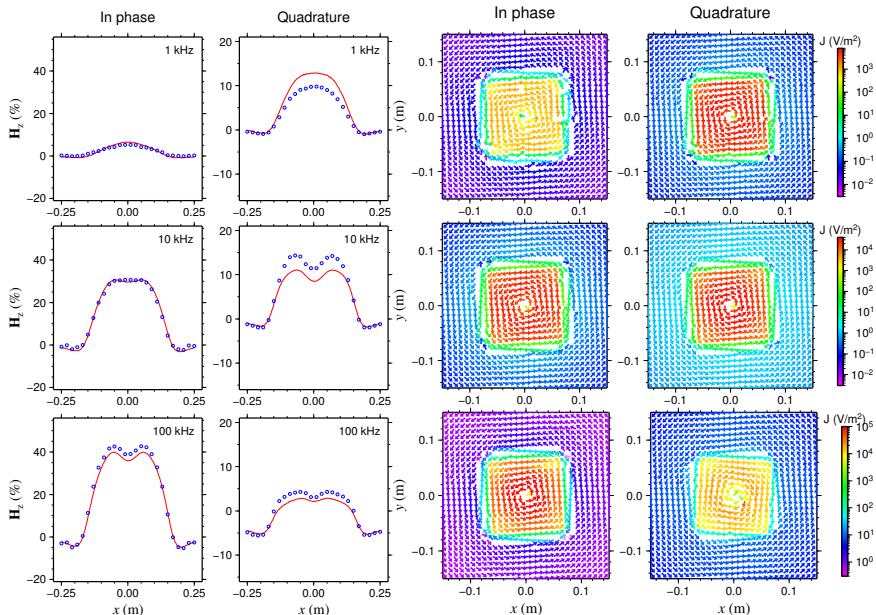


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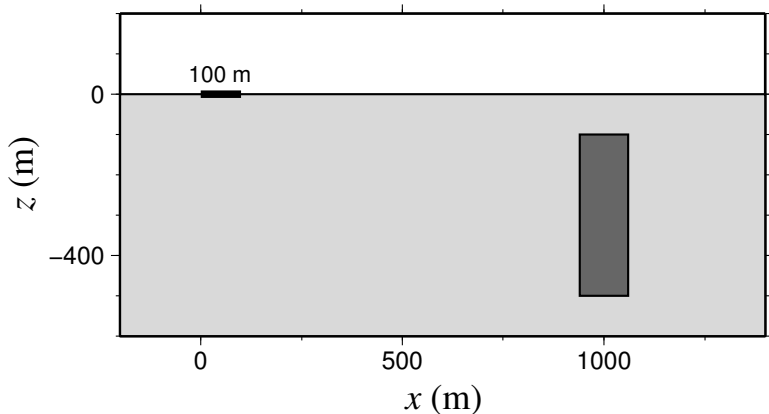


Example 1: magnetic dipole transmitter-receiver pairs



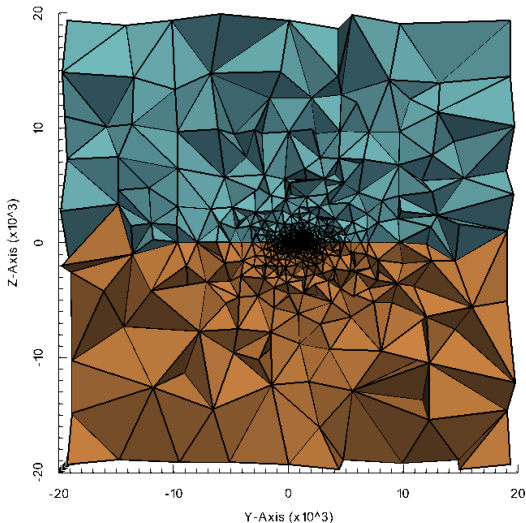
Example 2: long grounded wire

- 100 m wire along the x axis operating at 3 Hz
- Dimensions of the prism: $120 \times 200 \times 400$ m
- $\sigma_{ground} = 0.02$ S/m ; $\sigma_{prism} = 0.2$ S/m
- Observation points along the x axis



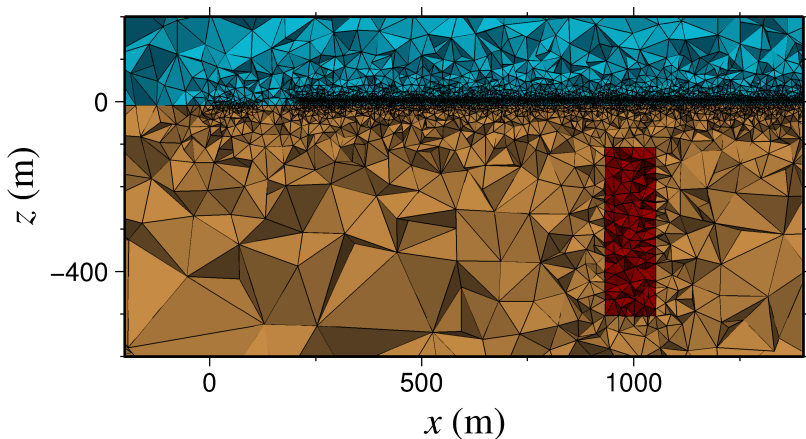
Example 2: long grounded wire

- Dimensions of the domain: $40 \times 40 \times 40$ km
- Number of tetrahedra: 162,689 ; number of unknowns: 189,105



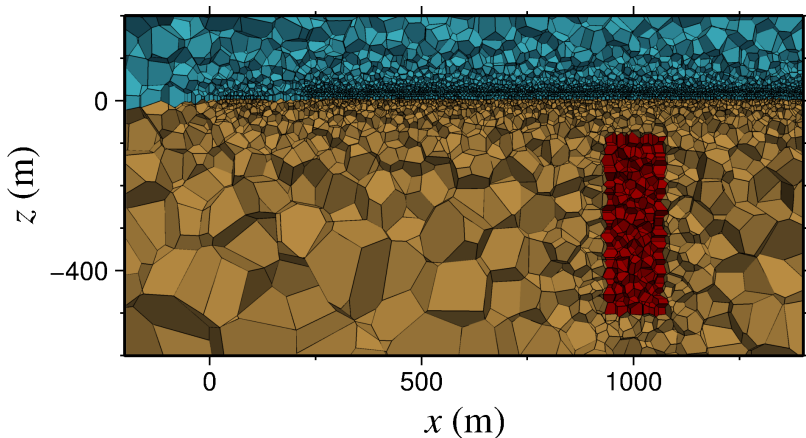
Example 2: long grounded wire

- Grid refined at the source, observation points and the prism
- Computation time: 40 s ; memory: 4 Gbytes (on Apple Mac Pro; 2.26 GHz Quad-Core Intel Xeon processor)



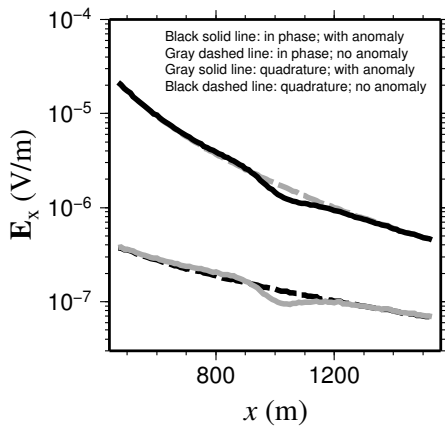
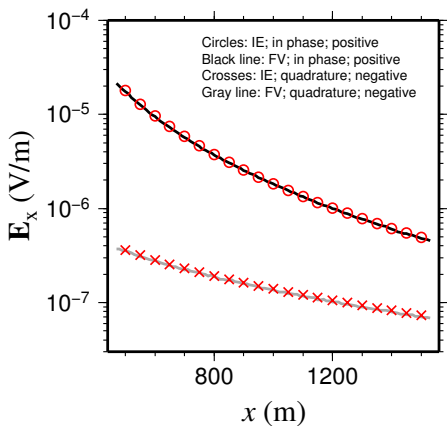
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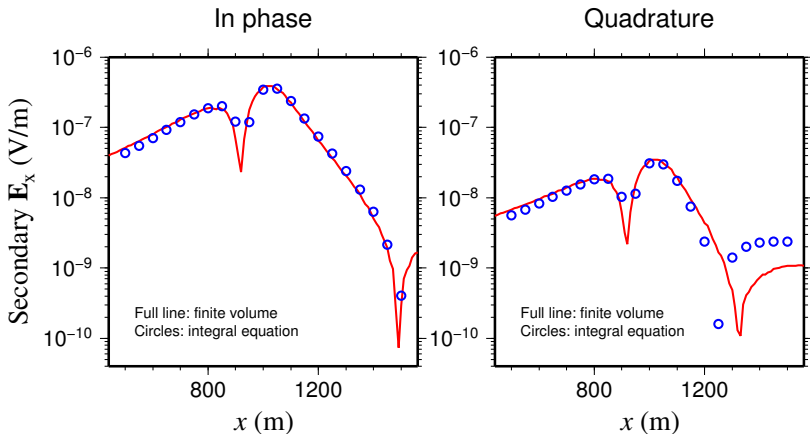
Example 2: long grounded wire

- Without prism (homogeneous halfspace)
- Total field
- FV vs IE (Farquharson and Oldenburg, 2002)
- With and without prism
- Total field
- FV only



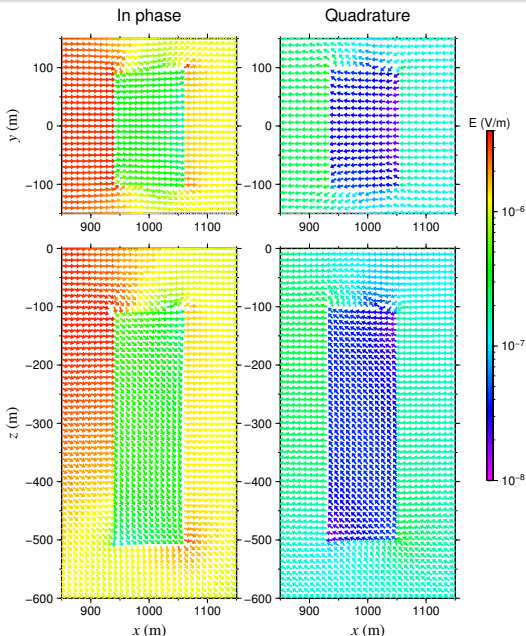
Example 1: long grounded wire

- Scattered field
- FV vs IE



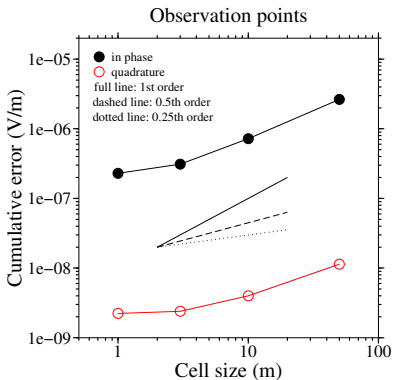
Example 2: long grounded wire

- Horizontal section ($z = -150 \text{ m}$)
- Total electric field (in phase and quadrature)
- Vertical section ($y = 0 \text{ m}$)
- Total electric field (in phase and quadrature)



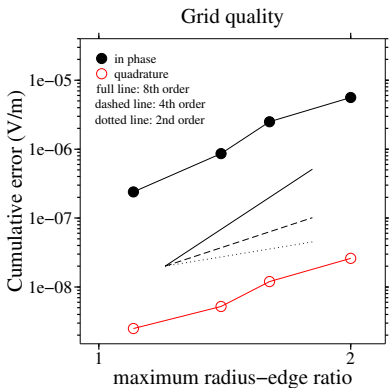
Example 2: accuracy studies

- Refinement at the observation points
- Exact solutions: solution due to a fine grid



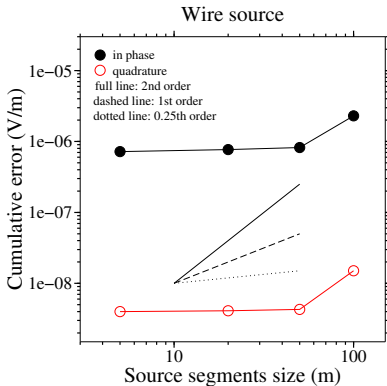
Example 2: accuracy studies

- **Improvement in grid quality**
- Quality criteria: maximum radius-edge ratio



Example 2: accuracy studies

- Refinement at the line source
- Line source divided into equal segments



- A finite-volume technique is used for modelling the total field EM data. This technique uses the staggered tetrahedral-Voronoi grid.
- The aim is making use of the features of unstructured grids for efficient modeling of the subsurface and for local refinements in the grid.
- The Helmholtz equation is discretized and solved using a sparse direct solver (MUMPS).
- The scheme has been tested for two models: one with a long grounded wire source; another one for magnetic source-receiver pairs with large conductivity contrasts.
- For the both examples, the results from the FV scheme are in good agreement with those from the literature.
- Accuracy studies show the relatively higher importance of refinement at the observation points and improvement in grid quality, and relatively lower importance of refinement at the sources.

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Atlantic Canada
Opportunities
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VALE

- Amestoy, P. R., Guermouche, A., L'Excellent, J. -Y. and Pralet, S., 2006. Hybrid scheduling for the parallel solution of linear systems, *Parallel Computing*, 32, 136156.
- Ansari, S. M., and C. G. Farquharson, 2013, Three-dimensional modeling of controlled-source electromagnetic response for inductive and galvanic components: Presented at the 5th International Symposium on Three-Dimensional Electromagnetics.
- Farquharson, C. G., and D. W. Oldenburg, 2002, An integral-equation solution to the geophysical electromagnetic forward-modelling problem, in *Three-Dimensional Electromagnetics: Proceedings of the Second International Symposium*: Elsevier, 319.
- Farquharson, C. G., Duckworth, K. and D. W. Oldenburg, 2006. Comparison of integral equation and physical scale modeling of the electromagnetic responses of models with large conductivity contrasts, *Geophysics*, 71, G169-G177.
- Si, H., 2004. TetGen, a quality tetrahedral mesh generator and three-dimensional delaunay triangulator, v1.3 (Technical Report No. 9). Weierstrass Institute for Applied Analysis and Stochastics.